



# FARNELL

INSTRUCTION MANUAL  
FOR

STABILISED VOLTAGE CURRENT  
SUPPLY UNITS

L30 SERIES

ISSUE 2

FARNELL INSTRUMENTS LTD. SANDBECK WAY, WETHERBY, YORKS.

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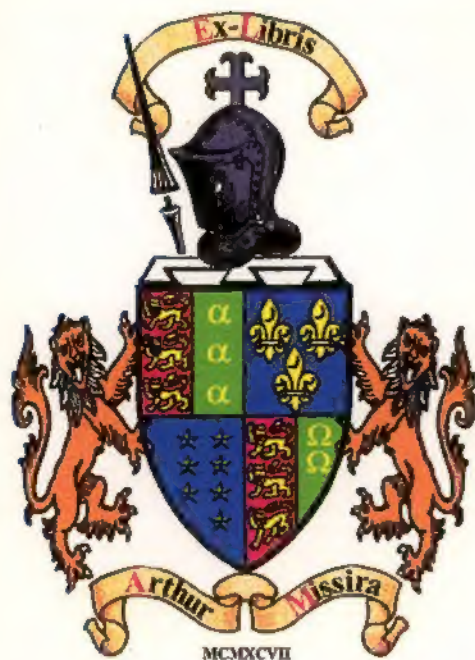
FARNELL INSTRUMENTS LIMITED

STABILISED VOLTAGE CURRENT  
SUPPLY UNITS

L30 SERIES

ISSUE 2

FARNELL INSTRUMENTS LTD.  
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## SECTION I

### INTRODUCTION

This manual covers the MK II L30 series of D.C. stabilised voltage/current supply units. The circuit diagram contained in the manual is for the particular unit type supplied.

Twin units are designated L30 -/T and consist of two appropriate L30 units mounted in the one case. The two outputs are completely independent. They may be used as separate supplies or alternatively may be connected in series or parallel, to provide higher output voltages or currents than can be obtained from a single L30 supply.

The semiconductor complement of these supplies is silicon throughout, permitting operation to 45°C ambient at full specified output.

The output voltage is adjusted by means of two controls on the front panel marked "COARSE" and "FINE."

The output voltage or current is monitored by a switched voltmeter/ammeter.

Overload protection is provided to protect the power unit and apparatus, being supplied by limiting the output current to a set value. This value is adjustable from zero to the maximum current of the unit by means of a control on the front panel marked "CURRENT LIMIT." The circuit will automatically reset when the overload is removed.

The instrument will operate from mains supplies of 210, 220, 230 and 240v. A.C. at 50/60 Hz.

(An alternative instrument is manufactured for use with mains supplies of 105—120v.).

Certain units in the range are fitted with internal overvoltage protection (see Section IV) when the unit output exceeds a level set by means of a front panel control, the unit output is clamped to a low value by means of a thyristor crowbar circuit.

## SECTION II

### OPERATING INSTRUCTIONS

Care should be taken to ensure that the input selector on the rear of the unit is set to match the mains supply from which the supply is to be operated.

The mains lead is wired as follows :—

BROWN Mains Line.  
BLUE Mains Neutral.  
GREEN/YELLOW Earth.

#### *NORMAL CONSTANT VOLTAGE OPERATION*

Before connection to the mains supply is made, the output "ON/OFF" switches, should be set to "OFF". The link on the bottom of the unit should be in the "CV" position.

With the mains supply connected, the mains "ON/OFF" switch is set to "ON" and the mains indicator lamp should light.

With the meter switch set to "VOLTS", the required output voltage is selected by adjusting the "COARSE" and "FINE" voltage controls on the front panel and the current limit control set to maximum (fully clockwise). Unless use of the current limiting is to be made, the load is now connected and the output "ON/OFF" switch set to "ON". Output current can be monitored by setting the meter switch to "CURRENT".

#### *CURRENT LIMIT SETTING*

If a certain maximum current must not be exceeded or a roughly constant current is required, use may be made of the current limiting facility, maximum current being set by the front panel control marked "CURRENT LIMIT".

#### *(1) APPROXIMATE CONSTANT CURRENT OPERATION*

With the mains supply connected to the unit, mains and output switches set to "ON", the meter switch set to "CURRENT" and the output voltage controls set to maximum, the positive output terminal is linked to the negative output terminal and the current limit control set to give the required current. On removal of the link and connection to the load, the unit will give a roughly constant current over a voltage range from zero to the maximum specified output voltage depending on the load resistance.

#### *(2) CURRENT CEILING OPERATION*

If a certain maximum current is not to be exceeded then the setting up procedure is as follows :—

With the mains supply connected to the unit, mains and output switches to "ON", the meter switch set to "CURRENT" and the voltage controls set to the required value, a variable load is connected to the unit and is set to give the required maximum current. The current limit control is then adjusted until the current just starts to fall. The unit will now prevent more current than this value being drawn from it. It is advised that this current "ceiling" is set to approximately 10% in excess of the expected maximum to prevent any modification to the voltage regulation characteristic. The variable load is now disconnected and the unit is ready for use.

#### *ACCURATE CONSTANT CURRENT OPERATION*

(See Fig. 1)

If a fixed resistor  $R_s$  is connected between the positive output terminal and the "I const" or "—F/B" terminal, the link on the bottom of the unit set to CI, and the load  $R_L$  between the "I const" or "—F/B" terminal and the "O/P - ve" terminal, then the unit will keep the voltage across  $R_s$  constant. Thus a constant current will flow in  $R_s$ . Since  $R_L$  is in series with  $R_s$ , the same current will flow in  $R_L$ .

The value of  $R_s$  is given by :—

$$R_s = \frac{V}{I_{out}} - R_L \text{ max.}$$

Where  $V$  is the maximum specified output voltage of the unit.

$R_s$  must have a power rating well in excess of the power it dissipates in order that the change in resistance due to self heating is minimised.

The power dissipated in  $R_s$  is given by :—

$$P(R_s) = I_{out}^2 R_s.$$

$R_s$  is then connected between the "O/P+" and "I const" terminals. The "I const" or "—F/B" terminal is shorted to the "O/P—" terminal and the "VOLTAGE ADJUST" controls set until the meter reads the required output current. The "short" is then removed and the load connected in its place. The output current will be constant with the same specification as the constant voltage specification with the load varying from zero to  $R_L \text{ max.}$

NOTE :—

The front panel "CURRENT LIMIT" control should be set to maximum for this mode of operation.

## FOUR TERMINAL OPERATION

Certain units have been provided with four terminal output to enable the correction of resistive drop in connecting leads. When this correction is not required, the +F/B and +O/P terminals should be linked together and the -F/B and -O/P terminals should be linked together. When correction is required the links should be removed. The load should be connected to the +O/P and -O/P terminals and the +F/B and -F/B terminals connected through separate wires to the appropriate ends of the load. It may be necessary to decouple at the load with an electrolytic capacitor to prevent instability in this connection.

## OVER-VOLTAGE PROTECTION

On units fitted with over-voltage protection the over-voltage trip level adjustment is on the front panel of the unit, and the current limit control on the back of the unit.

To set a given trip level, set the output voltage to this level, and adjust the "OVERVOLTAGE" control until the output voltage falls to a low level.

Set the voltage adjustment controls fully anti-clockwise, the output (or mains) switch to off, and then on. This resets the overvoltage trip. Re-adjust the output voltage controls to give the required operating voltage.

## SECTION III

### CIRCUIT DESCRIPTION

The circuit employs series regulator transistors driven via emitter followers from a differential amplifier which compares the voltage of a zener diode reference with a proportion of the output voltage derived from a resistive potential divider.

The mains supply is connected via fuse F1, SW1 and the input selector to MT1. The main secondary winding supplies a bridge rectifier, reservoir capacitor system which provides the main unregulated D.C. line. The positive line is connected via the series regulator transistors and SW2 to the positive output terminal. The negative line is connected via fuse F2 to the negative output terminal.

Supplies for the amplifier and reference section are derived from the auxiliary 36 volt secondary winding, via rectifier diodes D5 and D6 and smoothed by capacitor C2. The unstabilised reference line is fed to zener diode Z1 via resistor R2. The semi-stabilised voltage across Z1 is fed to zener diode Z2 and Z4 via R3 providing 10 volts positive and approximately 5 volts negative with respect to the positive output terminal. The voltage across Z2 feeds the reference zener diode Z3 and potential divider chain R7, T1, P1 and P2, via Resistor R4.

The base of VT1 and the negative of Z3 are connected to the positive output terminal. R7 and T1 are connected between the positive of Z3 and VT2 base via R8. Any difference between the voltages at VT1 and VT2 bases is amplified at the collector of VT2 and applied to VT3 base. After further amplification at VT3 collector the signal is applied to the emitter followers of the series regulator stage in such a sense as to oppose the original signal at VT1 and VT2 bases. The action of the loop is therefore to maintain zero voltage between VT1 and VT2 bases.

Output voltage is determined by :—

$$\frac{V_{ref} (P1 + P2)}{R7 + T1}$$

Overload protection is provided by VT4 and VT8. As output current increases, the voltage drop across R17 increases until the base of VT4 is sufficiently positive to turn it on. This diverts current from the series regulator stage, thus reducing the output voltage. On further increase in load, VT4 will maintain a roughly constant voltage drop across R17 which gives a roughly constant current output. The point at which the initial current limit occurs is set by P3 and the maximum current limit point is set by T2.

#### OVERVOLTAGE PROTECTION

On units fitted with overvoltage protection, this is provided by means of a Thyristor "crowbar" connected across the output terminals, and driven from a voltage comparator amplifier which compares a fraction of the output voltage with a reference zener diode. R1a, Z1a, R7a and VT1a, comprise a constant current source to feed the reference zener diode Z2a, Z9a and R10A feed a fraction of this voltage to VT3a base. VT3a and VT4a are the comparator transistors, the base of VT4a being fed from potential divider P1a, R6a and R13a. If the output voltage exceeds a level determined by this potential divider VT4a conducts, driving VT2a on. The drive then available from VT2a collector then fires SCR1a which short circuits the output terminal.

## SECTION IV

### SPECIFICATION

#### *Mains Supply*

210, 220, 230 or 240 volts 50/60 Hz.

Alternatively, instruments may be supplied for 105, 110, 120 volts 50/60 Hz.

#### *Output Voltage and Current Ranges*

##### SINGLE UNITS

L30A	0 — 50V.	0.5A.
L30B	0 — 30V.	1A.
L30C	0 — 10V.	3A.*
L30D	0 — 30V.	2A.
L30E	0 — 30V.	5A.
L30F	0 — 12V.	10A.*

##### TWIN UNITS

L30AT	2 × 0 — 50V.	0.5A.
L30BT	2 × 0 — 30V.	1A.
L30DT	2 × 0 — 30V.	2A.

\*Fitted with overvoltage protection.

#### *Mains Variation Tolerated*

± 10% of Nominal.

#### *Output Voltage Variation for ± 10% Mains Change*

Less than .01% or 1mV whichever is the greater—short term.

Less than .02% or 2mV whichever is the greater—long term.

#### *Output Voltage Variation for Zero to Full Load Change*

Less than .01% or 2mV whichever is the greater—short term.

Less than .02% or 4mV whichever is the greater—long term.

*Output Current Variation for 10% Mains Change (Accurate Constant Current Operation)*

Less than .01% or 1mA whichever is the greater—short term.

Less than .02% or 2mA whichever is the greater—long term.

*Output Current Variation for Zero Resistance to Max. Resistance Change (Accurate Constant Current Operation)*

Less than .01%—short term.

Less than .02%—long term.

*Output Current Variation for 10% Mains Change (Approximate Constant Current Operation)*

Less than 1%—short term.

Less than 2%—long term.

*Output Current Variation for Zero Res.—Max. Res. Change (Rough Constant Current Operation).*

Less than 2%—short term.

Less than 3%—long term.

*Ripple Voltage at Full Load*

Less than 1mV peak to peak.

*Ripple Current at Full Load*

Less than 1mA peak to peak.

*Overload Protection*

Current Limiting.

*Overvoltage Protection*

Thyristor "crowbar" trip. Trip level adjustment approx. 3.2V to 14V., temp. coefficient of trip level 0.04% /°C. typical.

*Max. Operating Temperature*

45°C.

*Temperature Coefficient*

±0.02% per °C. Typical.

*Output Impedance*

See Fig. (2).

## SECTION V

### INTERNAL ADJUSTMENT

Units are set up before leaving the factory, but in the event of future mis-alignment the setting-up procedure is as follows:—

#### *VOLTAGE ADJUSTMENTS*

(1) An accurate voltmeter is connected between the "O/P—" and "O/P+" terminals, with an f.s.d. compatible with the specified maximum output voltage of the unit.

With the unit switched on, the link on the bottom of the unit set to "CV" and the "VOLTAGE ADJUST" controls fully clockwise, T1, on the circuit board, is adjusted to give the specified maximum output voltage.

(2) With the meter switch set to "VOLTS", T3 is now adjusted so that the front panel meter reads full scale.

#### *CURRENT ADJUSTMENTS*

(1) An accurate ammeter with an f.s.d. compatible with the specified maximum output current of the unit, is connected in series with a variable load between the "O/P+" and "O/P—" terminals.

With the unit switched on, the link on the bottom of the unit set to "CV" and the "CURRENT LIMIT" control fully clockwise, the load is adjusted to give 10% in excess of the specified maximum output current. T2 is then adjusted until the current just starts to fall.

(2) With the meter switch set to "AMPS", the load is re-adjusted to give the specified maximum output current and T4 is adjusted so that the front panel meter reads full scale.

## SECTION VI

### TYPICAL PERFORMANCE AND APPLICATIONS

#### 1. VOLTAGE PROGRAMMING

All units can be programmed by means of external resistors to any voltage below the specified maximum voltage, the programming terminal being the "I const" or "—F/B" terminal. The link on the bottom of the unit is set to "CI" and the "VOLTAGE ADJUST" controls turned fully anticlockwise. The programming resistor should now be connected between the "I const" and "O/P—" terminals.

The value of programming resistor is given by :—

$$R_{\text{prog}} = \frac{25.25}{50} \times V_{\text{required}}, \text{ Kilohms (L30A)}$$

$$R_{\text{prog}} = \frac{25.25}{30} \times V_{\text{required}}, \text{ Kilohms (L30B, D \& E)}$$

$$R_{\text{prog}} = \frac{5.1}{10} \times V_{\text{required}}, \text{ Kilohms (L30C)}$$

The tolerance on  $V$  required for an accurate  $R_{\text{prog}}$  is  $\pm 10\%$ . In order to obtain greater accuracy, the voltage of the reference zener-diode  $Z3$ , ( $V_{\text{ref}}$ ) and the resistance of  $R7 + T1$  must be determined.  $R_{\text{prog}}$  is now given by :—

$$R_{\text{prog}} = \frac{R7 + T1}{V_{\text{ref}}} \times V_{\text{required}}, \text{ ohms}$$

The tolerance on  $V$  required for an accurate  $R_{\text{prog}}$  is now the tolerance on the  $V_{\text{ref}}$  measurement plus the tolerance on the  $R7 + T1$  measurement.

#### 2. SERIES OPERATION

Units may be connected in series ONLY IN THE "CV" MODE OF OPERATION.

#### 3. PARALLEL OPERATION

##### (A) "CV" OPERATION

Units which are set to approximately the same output voltage may be connected directly in parallel. On increasing load, the unit having the highest output voltage will carry the load until it current limits, thereafter the unit having the next highest

voltage will supply the extra current until it limits, and so on. A typical output characteristic for a parallel combination of three units is shown in Fig. (3).

The characteristic shows a series of descending steps in output voltage at the current limit points of individual units, the amplitude of the steps depends on how closely the output voltages have been set and it may not be possible to adjust this to better than 50mV.

It is recommended that not more than three units are paralleled in this way.

##### (B) "CI" OPERATION

Units can be connected directly in parallel in either "APPROXIMATE CI" or "ACCURATE CI" operation, the load current being the sum of the two output currents, Fig. (I) shows the connections for "ACCURATE CI" operation.

#### 4. TYPICAL PERFORMANCE

##### Stability

Output variations are due in the main to the following causes :—

Load Change.

Mains supply change.

Component temperature change.

##### (a) Load Change

(I) Steady load—For a change in steady load from zero to full load, the typical change is :— 1mV at full voltage output.

(II) Transient Response—The typical response to a pulsed load is shown in Fig. (4).

##### (III) Output Impedance.

For alternating load superimposed on a steady load, the output impedance of the supply increases with frequency due to the fall off in gain of the amplifier until it is determined only by the capacitor across the output terminals.

A typical output impedance/frequency curve is shown in Fig. (2)

### (b) Mains Supply Change

Short term mains variations of up to 10% give corresponding variations of up to 0.01% on the output. Surges on the mains supply in the form of short rise time pulses can be fed on to the output by stray capacity. Where these conditions exist a capacitor suppressor filter should be connected in the mains lead.

### (c) Component Temperature Change

Output variation is caused by component value changes due to temperature change. The temperature change can be (I) as a result of ambient change, or (II) as a result of unit internal temperature change, caused by changing internal dissipation from a change in load or supply to the unit.

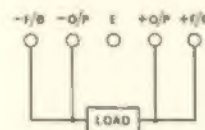
(I) Ambient Change—The typical temperature co-efficient of output voltage is .02% per degree centigrade of ambient change.

(II) Internal Change—Fig. (5) shows typical output variations caused by mains change and load change plotted against time.

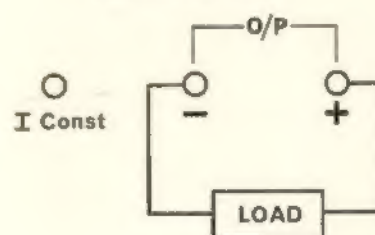
#### CONSTANT VOLTS

Link to "CV"

Four Terminal Units



Three Terminal Units



#### CONSTANT CURRENT

Link to "CI"

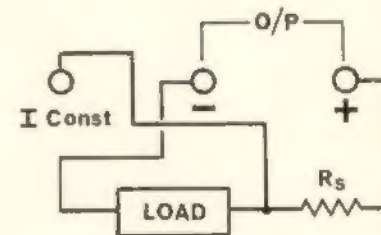
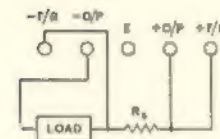


Fig. 1. CV and CI Connections

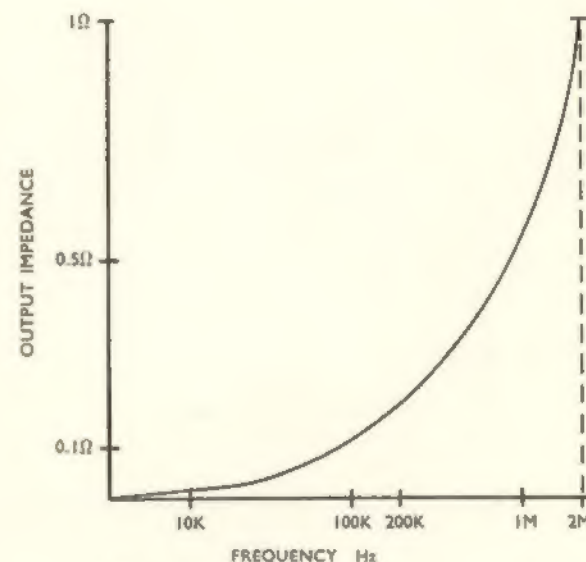


Fig. 2. Output Impedance

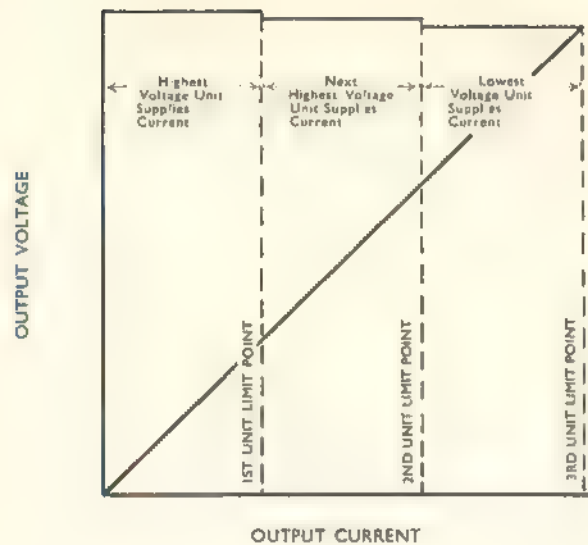


Fig. 3. Parallel Operation

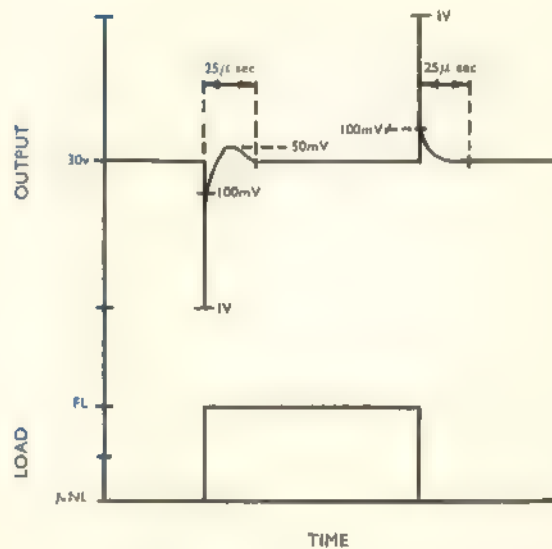


Fig. 4. Pulse Response

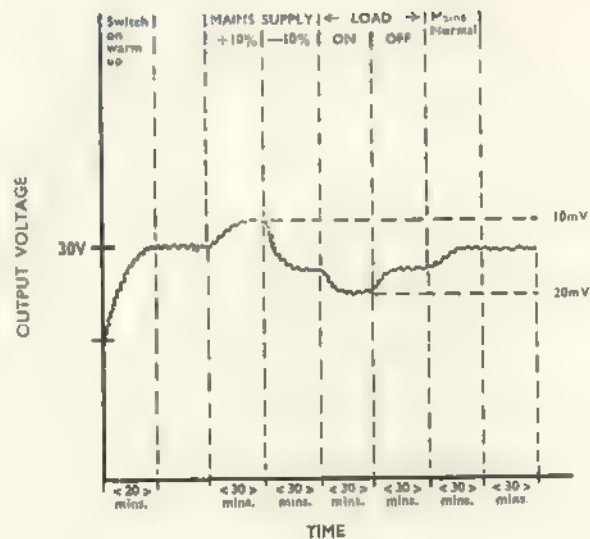


Fig. 5. Typical Output Voltage Variation against Time

## ERRATA AND ADDENDA

ALTERNATIVE COMPONENTS TO THOSE LISTED ON CIRCUIT DIAGRAM MAY BE USED IN THE EVENT OF SUPPLY DIFFICULTIES. MAJOR CHANGES TO THE DESIGN OR MANUAL ARE LISTED BELOW:—

DRAWING No. 3-2808

SHEET 1 OF 2

ENTS LTD. WETHERBY, YORKS.

DRAWING No. 3-3069

SHEET 2 OF 2

ENTS LTD. WETHERBY, YORKS.

SPINDLE LENGTH 3/8"

USED ON		LOCATION	COMPONENT NUMBER	QUANTITY	VALUE	TOLERANCE	MANUFACTURER	MANUFACTURER'S TYPE No	MANUFACTURER'S RATING	OPERATIONAL RATING (MAX)	REMARKS	LOCATION	COMPONENT NUMBER	QUANTITY	VALUE	TOLERANCE	MANUFACTURER	MANUFACTURER'S TYPE No	MANUFACTURER'S RATING	OPERATIONAL RATING (MAX)	REMARKS
BP	F1	1	2A			BESWICK	TDC134														
"	F2	2	2A			"	TDC 69														
FP	SW1	1				PAINTON	100123														
"	SW2	2				"	"														
"	SW3	2				"	"														
CH	MT1	2																			
FP	MI	2				SIFAM	CLARITY42														
"	NI	1				ARCOELECTRIC	SL268														

TRACED

CHECKED

DRAWN *RES.*

ISSUE 1

DATE 25-7-68

MOD No

LOCATION KEY

FP: FRONT PANEL

BP: BACK PANEL

CH: CHASSIS

SERIAL NUMBER

TESTED

DATE

FARNELL INSTRUMENTS LTD, WETHERBY, YORKS.

TITLE:—

CIRCUIT DIAGRAM KEY

L30DT

DRAWING No. 3-3060/K

SHEET 2 OF 2 SHEETS

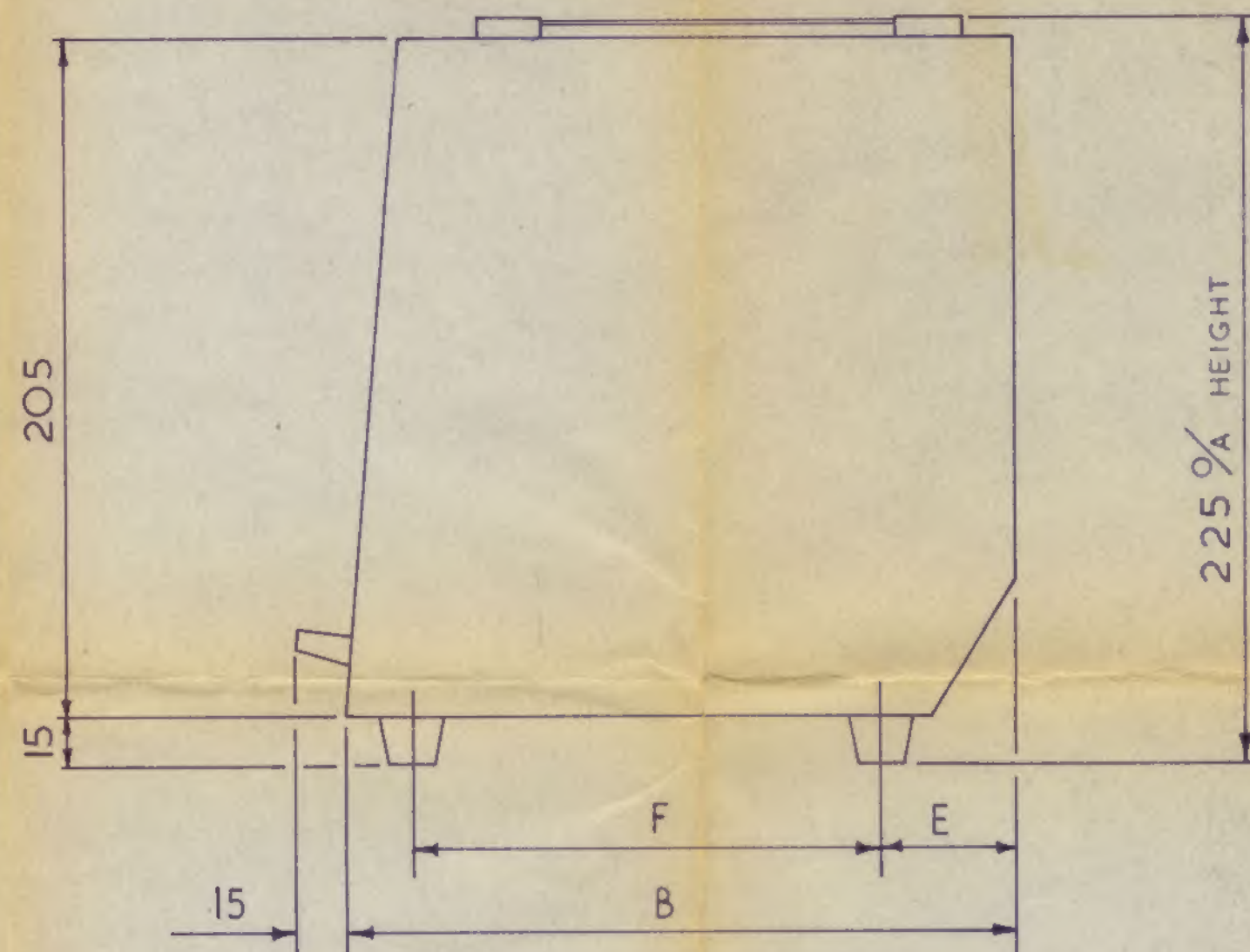
USED ON		LOC. TION	COMPO- NENT NUMBER	QUAN- TITY	VALUE	TOLERANCE	MANUFACTURER	MANUFACTURER'S TYPE No.	MANUFAC- TURER'S RATING	OPERA- TIONAL RATING (MAX.)	REMARKS	LOC. TION	COM- PONENT NUMBER	QUAN- TITY	VALUE	TOLERANCE	MANUFACTURER	MANUFACTURER'S TYPE No.	MANUFAC- TURER'S RATING	OPERA- TIONAL RATING (MAX.)	REMARKS											
		CBI	R1	2	3.3K $\Omega$	5%	ELECTROSIL	TR6				H.S.	VT7	2				RCA	2N3055													
		"	R2	2	1.2K $\Omega$	"	WELWYN	W21				CBI	VT8	2				TEXAS	BC182L													
		"	R3	2	180 $\Omega$	"	ELECTROSIL	TR5				HS	VT9	2				RCA	2N3055													
		"	R4	2	1.2K	"	"	"				"	VT10	2				"	"													
		"	R5	2	8.2K $\Omega$	"	"	"				"	VT11	2				"	"													
		"	R6	2	4.7K $\Omega$	"	"	"																								
		"	R7	2	3.3K	"	"	"																								
		"	R8	2	47 $\Omega$	"	"	"																								
		"	R9	2	150 $\Omega$	"	"	"																								
		"	R10	2	39 $\Omega$	"	"	"																								
		"	R11	2	3.3K $\Omega$	"	"	"				CBI	D1	2				TEXAS	IN4721													
		"	R12	2	5.0T.	"	"	"				"	D2	2				"	"													
		H.S.	R13	2	330 $\Omega$	"	"	"				"	D3	2				"	"													
		"	R14	2	120 $\Omega$	"	"	"				"	D4	2				"	"													
		CBI	R15	2	27K $\Omega$	"	"	"				"	D5	2				MULLARD	BYX36/300													
		"	R16	2	560 $\Omega$	"	"	"				"	D6	2				"	"													
		CH	R17	2	0.5 $\Omega$	"	WELWYN	W21				"	D7	2				TEXAS	IN659													
		CBI	R18	2	10K $\Omega$	"	ELECTROSIL	TR5				"	D8	2				"	"													
												"	D9	2				"	IN4721													
												"	D10	2				MULLARD	BYX36/300													
		CBI	R20	2	1.2K $\Omega$	5%	ELECTROSIL	TR6																								
		H.S.	R21	2	0.5 $\Omega$	"	WELWYN	W22																								
		"	R22	2	"	"	"	"																								
		"	R23	2	"	"	"	"																								
		"	R24	2	"	"	"	"																								
												CBI	Z1	2				I.R.C.	MZ18T5													
												"	Z2	2				"	MZ10T5													
												"	Z3	2				EMIUS	HS2051													
												"	Z4	2				"	"													
		CBP	C1	1	2200 $\mu$ F		HUNTS	KA3132	63V																							
		CBI	C2	2	32 $\mu$ F		MULLARD	C426ARH32	64V																							
		"	C3	2	1000pF		WIMA	TFF	400V																							
		"	C4	2	4.7 $\mu$ F		SIEMANS	MKL	63V																							
		CH	C5	4	220 $\mu$ F		ELECTRAUTON	454	40V		ALL 400V.40	CBI	T1	2	2.2K $\Omega$		PLESSEY	WMP														
		C.B.	C6	2	1000pF		WIMA	TFF	400V			"	T2	2	2.2K $\Omega$		"	WMP														
		FP	C7	2	330pF		WIMA	TFF	400V			"	T3	2	5.6K $\Omega$		"	MP														
		"	C8	2	0.1 $\mu$ F		"	TFM	160V			"	T4	2	1K $\Omega$		"	MP														
			C10	2	0.22 $\mu$ F		"	TFM	160V																							
			C11	2	1000pF		"	TFM	400V																							
		CBI	VT1	2			TEXAS	2N3702																								
		"	VT2	2			"	"																								
		"	VT3	2			"	BC182L																								
		"	VT4	2			"	"				FP	P1	2	25K		A.B.METALS	43			SPINDLE LENGTH 3/8"											
		"	VT5	2			"	2N3053				"	P2	2	250 $\Omega$		"	"														
		CBS	VT6	2			RCA	2N3055				"	P3	2	1K $\Omega$		"	"														
TRACED												LOCATION KEY																				
		4	11.9.69	628		10	7.7.70	776	CBI - CIRCUIT BOARD												F.P. - FRONT PANEL		FARNELL INSTRUMENTS LTD, WETHERBY, YORKS.									
CHECKED		3	28.8.68	626		9	19.5.70	765	CBP - "																							

### THIRD ANGLE PROJECTION

ALL ERRORS TO BE REPORTED TO THE DRAWING OFFICE

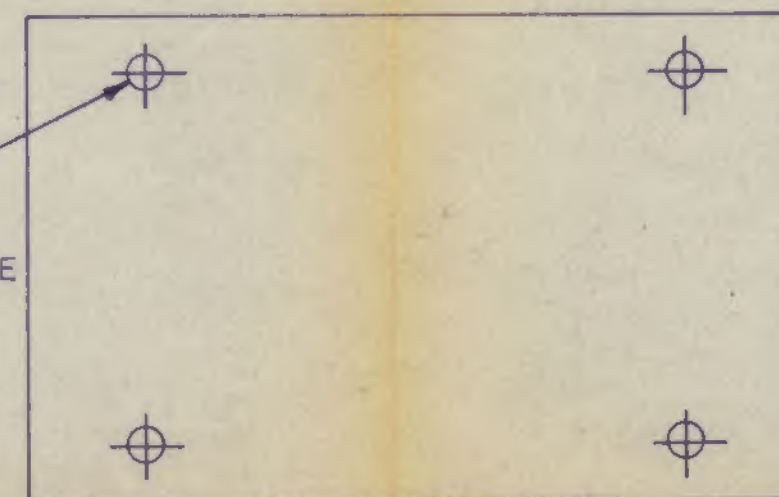
USED ON

1242



	A	B	C	D	E	F	WEIGHT	
							LBS	Kg.
L30A L30B L30C	132	205	17	98	41	142	8.5	3.86
L30AT L30BT	255	205	12.75	221.5	41	142	16	7.26
L30D	132	230	17	98	66	142	9	4.08
L30E L30F	228	248	19	190	49	180	17.75	8.06
L30DT	255	230	12.75	221.5	66	142	17	7.71

4X4BA SCREWS  
SECURING FEET  
NOTE NUTS ON BASE  
ARE NOT CAPTIVE  
ie INSIDE UNIT

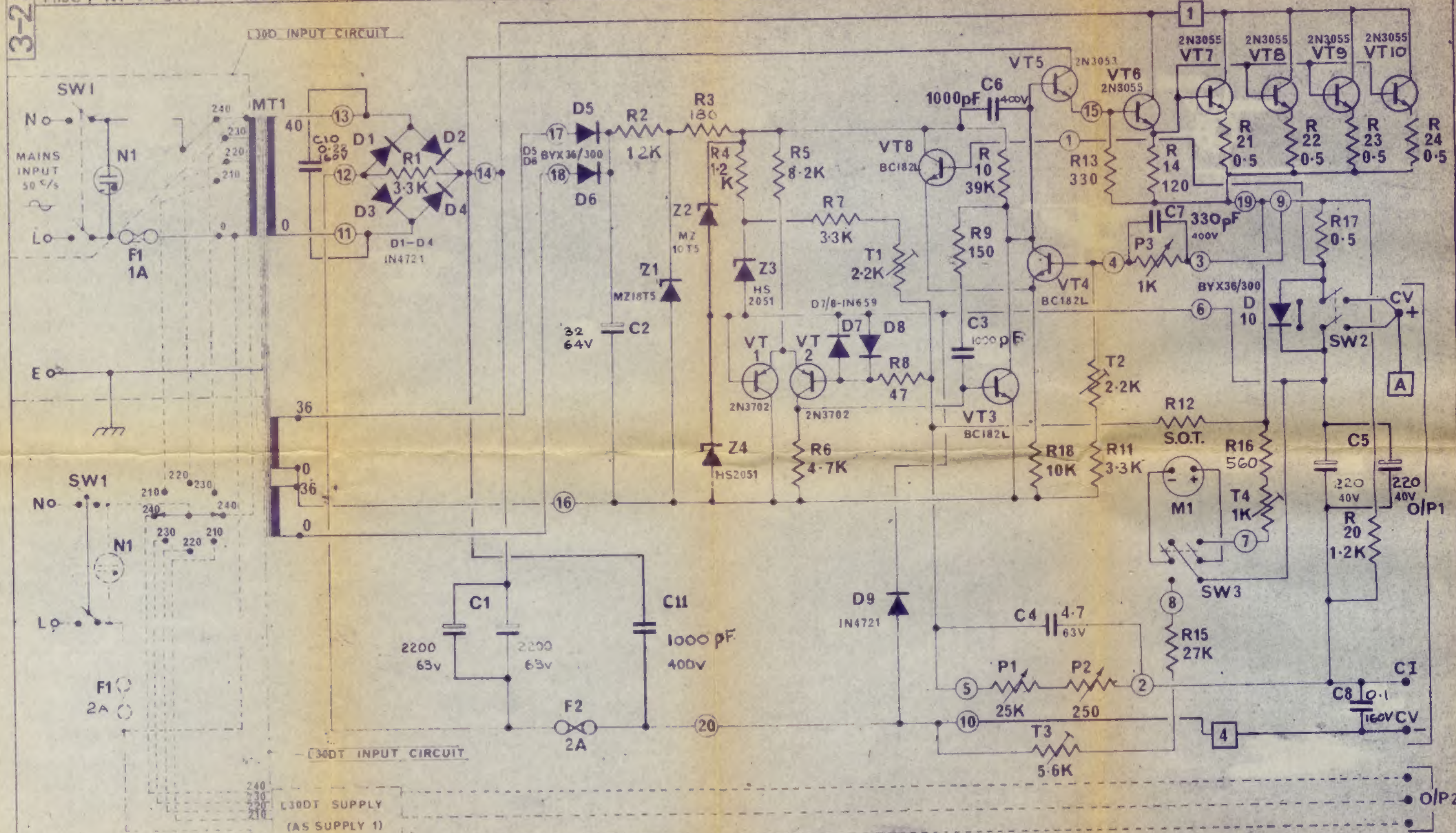


TRACED						TOLERANCES	PROTECTIVE FINISH	NOTE : REMOVE ALL BURRS AND SHARP EDGES	FARNELL INSTRUMENTS LTD. WETHERBY, YORKS.	
CHECKED						MATERIAL			TITLE :  MECHANICAL SPECIFICATION L30 SERIES	DRAWING No.  3-2808
DRAWN M H	ISS. 1	DATE 15.2.69	MOD. No.			SCALE :				DIMENSIONS IN M.M.

USED ON

3-2810

R		1		2	3	4	5	6	7	8	9	10	18	11	13	14	15	12	21	16	22	17	23	24	20	R				
C		10		1		2		11			3	6	4			7				5	8					C				
VT							1	2		8		3	4	5		6		7		8		9	10			VT				
MISC	N1	F1	SW1	MT1	D1	D3	D2	D4	F2	D5	D6	Z1	Z2	Z3	Z4	D7	D8	T1	D9	P1	T3	P2	T2	P3	M1	SW3	T4	D10	SW2	MISC



NOTE POINTS 1, 4 & A OVER VOLTAGE TRIP CONNECTIONS (WHEN FITTED)

TRACED	5	11-9-69	628	10	5-5-70	150		
CHECKED	3	8-8-69	512	9	14-4-70	757	15	3-2-71
	2	5-2-70	570	8	10-3-70	752	14	27-10-70
DRAWN	ISS.	DATE	MOD. No.	7	11-2-70	733	13	21-9-70
	1			6	11-10-69	658	12	7-7-70

NOTE —  
CAPACITOR VALUES GIVEN IN µF  
RESISTOR VALUES IN Ω  
② REFERS TO CCT. 80.  
PIN CONNECTION Nos.

FARNELL INSTRUMENTS LTD. - WETHERBY, YORKS

CIRCUIT DIAGRAM

L30D & L30DT

DRAWING No.

3-2810

